PAPER • OPEN ACCESS

Study of hydrogen concentration in the weld seam during welding of mining equipment

To cite this article: A A Usoltsev et al 2021 IOP Conf. Ser.: Earth Environ. Sci. 823 012029

View the article online for updates and enhancements.



This content was downloaded from IP address 62.231.181.231 on 17/08/2021 at 02:27

IOP Conf. Series: Earth and Environmental Science 823 (2021) 012029 doi:10.1088/1755-1315/823/1/012029

Study of hydrogen concentration in the weld seam during welding of mining equipment

A A Usoltsev, N A Kozyrev, A R Mikhno, R E Kryukov and V Ya Tsellermayer

Siberian State Industrial University, 42 Kirova, Novokuznetsk, 654007, Russia

E-mail: kozyrev na@mtsp.sibsiu.ru

Abstract. The study of the hydrogen content in the weld during the welding of mining equipment was carried out. It was found that with an increase in current strength, voltage and welding rate, a decrease in the hydrogen concentration in the welded joint of the samples is possible. The obtained welded samples meet the requirements for the hydrogen content - the hydrogen concentration in all samples is less than $2 \text{ cm}^3/100\text{g}$.

1. Introduction

Submerged arc welding is the leading technological process in the manufacture of large-sized welded metal structures of mining equipment. At the same time, an important direction in welding production is the development of new welding fluxes that provide the required physical and chemical parameters with a lower cost [1-4]. The solution to this problem can be found through the use of metallurgical production waste as welding fluxes, which, along with the costs reduction in the manufacture of fluxes, increase the quality of the weld by reducing the concentration of hydrogen [5-8].

Earlier, in previous works, the possibility of using silicomanganese slag as welding fluxes was considered [9-13]. The study of the influence of welding modes on the hydrogen content in welded seams was carried out using the equipment of the Scientific and Production Center "Welding Processes and Technologies".

2. Research methods

In this study, for the welded structures of mining equipment made of steel 09G2S, we used slag from the production of silicomanganese fraction from 0.45 to 2.5 mm with the chemical composition shown in table 1.

Table 1. (Chemical	composition of	of the flux	based on t	the slag p	roduced by	silicomanganese.
------------	----------	----------------	-------------	------------	------------	------------	------------------

Mass fraction of elements, %												
FeO	MnO	CaO	SiO ₂	Al ₂ O ₃	MgO	S	Р	ZnO	С	F	TiO ₂	Cr_2O_3
0.42	16.22	29.00	41.34	6.53	1.33	0.24	0.022	0.008	0.031	0.31	0.15	0.025

When developing the technology, the welding of the samples was carried out after drying the welding flux at a temperature of 250-300 °C for 3 hours, using steel plates of 09G2S steel 20 mm thick by Sv-08GA welding wire using an ASAW-1250 automatic welding tractor. Welding modes of samples were selected by the method of full-factor mathematical planning of the experiment. The obtained samples were investigated for chemical composition by the X-ray fluorescence method on the XRF-1800 spectrometer and by the atomic emission method on the DFS-71 spectrometer. The



IOP Conf. Series: Earth and Environmental Science 823 (2021) 012029 doi:10.1088/1755-1315/823/1/012029

determination of the chemical composition of the weld metal was carried out by chemical methods: for carbon content according to GOST 12344-2003, sulfur according to GOST 12345-2001 and phosphorus according to GOST 12347-77.

3. Results and discussion

When developing the technology for producing welded joints with low gas saturation, the hydrogen concentration in the weld was also determined. Measurements of the hydrogen content in the welded seam were carried out on a Gasochrome 3101 chromatograph.

The modes of welding the samples are presented in table 2. For welding the reference sample, the following mode was used: 700A-30B-30 cm/min. The chemical composition of the welds is shown in table 3.

Table 2. Modes of welding samples.												
Experiment			Current				Voltage, V			Velding	Heat input,	
number			strength, A							cm/m	J/cm	
0 (comparison sample)			700			30			30			42000
1			600			28			28			36000
2			600			30			32			33750
3			600			32			30			38400
4			650			28			32			34125
5			650			30			30			39000
6			650				32			28	44571	
7			700			28			30			39200
8			700			30			28			45000
9			700			32			32			42000
Table 3 Chemical composition of welds												
		Mass fraction of elements, wt%										
Sample No.	С	Si	Mn	Cr	Ni	Cu	Ti	Mo	Al	S	Р	H, cm ³ /100g
0	0.11	0.41	1.16	0.05	0.31	0.15	0.002	0.10	0.009.	0.014	0.014	1.1
1	0.07	0.48	1.24	0.05	0.43	0.16	0.001	0.14	0.012	0.013	0.016	1.2
2	0.08	0.54	1.38	0.06	0.28	0.17	0.17 0.003 0.08		0.018	0.014 0.014		1.1
3	0.08	0.51	1.31	0.06	0.32	0.15 0.001 0.10		0.014	0.014	0.013	1.4	
4	0.08	0.49	1.20	0.05	0.45	0.17 0.002 0.16		0.013	0.011 0.015		1.1	
5	0.07	0.50	1.26	0.05	0.43	0.17	0.17 0.003 0.14		0.002	0.012	0.018	1.1
6	0.07	0.49	1.25	0.05	0.40	0.16	0.16 0.002 0.13		-	0.012	0.015	1.0
7	0.09	0.50	1.23	0.04	0.41	0.13	0.13 0.001 0.14		0.014	0.011	0.011	1.3
8	0.09 0.50 1.31 0.06 0.31 0.17 0.001 0.0		0.09	0.019	0.014	0.013	1.0					
9	0.07	0.53	1.27	0.05	0.37	0.15	0.002	0.12	0.010	0.015	0.016	0.9

All selected samples meet the requirements for hydrogen content – hydrogen concentration in all samples is less than 2 cm³/100g. The dependences of the hydrogen content in the weld on the welding modes are shown in figures 1-3.

The use of mathematical and statistical methods made it possible to construct a mathematical model of the influence of technological modes (current strength, voltage during welding, welding speed) on the hydrogen content in the weld. Regression analysis of the influence of the welding modes of the samples, with the parameters: I - current strength, A; U - voltage, V; V is the welding rate, cm/min; E - heat input, J/cm is represented by the following equations:

For hydrogen: H2, $(cm^3/100g) = 3.26+0.02274 \cdot I+0.504 \cdot V-0.000406 \cdot E$; R2 = 0.70378

For hydrogen, taking into account heat input:

IOP Conf. Series: Earth and Environmental Science 823 (2021) 012029 doi:10.1088/1755-1315/823/1/012029

H2, $(cm^3/100g) = -20.0253+0.0526 \cdot I+1.1505 \cdot U-0.001193 \cdot I \cdot U-0.4094 \cdot V-0.000307 \cdot E$; R2 = 0.97092 The hydrogen content in the welds indicates that, other things being equal, the hydrogen concentration depends on the amperage, voltage and welding speed. The dependences of the hydrogen content in the weld on the welding modes are shown in figures 1-3.



Figure 1. Dependence of the hydrogen content in the welds on the change in the electric current during welding.



Figure 2. Dependence of the hydrogen content in welded joints with a change in welding voltage.



Figure 3. Dependence of hydrogen content in welds with changing welding rate.

4. Conclusion

According to the results of the studies carried out, the data were obtained on the effect of welding modes on the hydrogen content in the weld. It was found that with an increase in current strength, voltage and welding rate, it is possible to reduce the hydrogen concentration in the weld.

IOP Conf. Series: Earth and Environmental Science 823 (2021) 012029 doi:10.1088/1755-1315/823/1/012029

The obtained welded samples meet the requirements for the hydrogen content – the hydrogen concentration in all samples is less than $2 \text{ cm}^3/100\text{g}$.

References

- Brusnitsyn Yu D and M Yu Brusnitsyn 2000 Use of Phase Equilibrium Diagrams of Nonmetallic Systems for Diagnostics and Development of Welding Consumables (St. Petersburg: TsNII KM "Prometey") p 41
- [2] Kartashev M F, Naumov S V et al 2018 Proc. of Int. Sci. and Tech. Youth. Conf. (Tomsk) pp 174–175
- [3] Kalinnikov V T, Nikolaev A I and Malyshevsky V A 2009 *Proc. of the Int. Sci. and Tech. Conf. Petraniev Readings: "Welding Materials"* (St. Petersburg) pp 80-89
- [4] Kokorin V N 2003 Economy, Ecology and Society of Russia in the 21st Century (SP-b TSU) pp 273–274
- [5] Kozyrev N A and Kryukov R E 2017 Innovations in the Fuel and Energy Complex and Mechanical Engineering (Kemerovo) pp 128–133
- [6] Kislov A I, Mikhno A R and Kozyrev N A 2018 Proc. of the All-Russian Sci. Conf. of Students, Postgraduates and Young Scientists (Novokuznetsk: SibSIU) pp 208-210
- [7] Mikhno A R, Kryukov R E et al 2019 Welding in Russia 2019: Current State and Prospects: Abstracts of the International Conference (Tomsk) pp 187–188
- [8] Kozyrev N A and Kryukov R E 2017 Innovations in the Fuel and Energy Complex and Mechanical Engineering (Kemerovo) pp 134-139
- [9] Kozyrev N A, Kryukov R E et al 2016 *IOP Conf. Series: MSE* **150** 012032
- [10] Kozyrev N A, Kryukov R E et al 2016 IOP Conference Series: MSE 125 012034
- [11] Kozyrev N A, Mikhno A R et al 2018 IOP Conference Series: EES 206 012032
- [12] Kryukov R E and Kozyrev N A 2019 Fundamentals of Creating Carbon-containing Welding and Surfacing Materials (Tomsk: TPU) p 359
- Kozyrev N A, Mikhno A R et al 2019 Metallurgy: Technology, Innovation, Quality. Metallurgy (Novokuznetsk) pp 322–328