Materials and Processing Technology

Edited by Dmitry A. Chinakhov

Materials and Processing Technology

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Preface

Intensive development of engineering contributes to the emergence of new materials and technologies for their processing. This special issue contains research papers on modern technologies for obtaining and processing materials, technologies for obtaining welded joints, additive technologies.

The book is intended for a wide range of specialists engaged in the development and production of heavy-duty metal structures, as well as students, undergraduates, graduate and postgraduate students of technical colleges and universities.

Dmitry A. Chinakhov, PhD, Vice-Chancellor, Yurga Institute of Technology of National Research Tomsk Polytechnic University

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Abrasive Wear Resistance Comparative Analysis of the Metal Surfaced by Flux Cored Wires Systems Fe-C-Si-Mn-Ni-Mo-W-V and Fe-C-Si-Mn-Cr-Ni-Mo-V

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Keywords: flux cored wire, abrasive-shock wear, surfacing, recovering, wear resistance, hardness, nonmetalic incusions, structure.

Abstract. In the article is shown the comparative analysis between structures of surfaced by the flux coded wire metal systems Fe-C-Si-Mn-Cr-Ni-Mo-V and Fe-C-Si-Mn-Ni-Mo-W-V. These powder wires are supposed to be used in recovering details and equipment components and machines, that works in conditions of intensive abrasive – shock wear. Manufacturing and surfacing of flux cored wires samples were made in laboratory conditions. Defined chemical composition of the surfaced metal. Deposited metal samples hardness and wear resistance were researched. In the course of deposited meta surface metallographic analysis were made following metallographic researches: defined nature and level of nonmetallic oxides impurity, type and morphology of the microstructure, grain size of surfaced samples. Estimation of the chemical composition components influence on the hardness and wear resistance were obtained.

Introduction

Developing new materials and innovation recovering technologies, that extremely increase items wear resistance property, is the current problem in engineering. For these purpose development and manufacturing of specialized methods and materials of surfacing is in progress [1-16]. Most popular for surfacing detail which works in abrasive wear conditions is flux cored wire for surfacing of low-carbon and low-allow type, austenitic and high-manganese type C, and rapid steels type F per IIC classification [17]. Also, surfacing carbide allows type P have a widespread use, that constitute composite materials, and comprise reinforcing tungsten carbide elements and matrix. They are notable for high wear resistance in abrasive-shock wear conditions [17]. The characteristic feature in the wearout prosses for such allows is stepwise separate elements wearout of composition. In that case appears what is known as shading affect, when most wear resistance reinforcing elements took all major pressure from destructive force on itself, protecting allow matrix from wearout. Then, while matrix wear resistance is in balance its components working capacity could be defined by its chemical composition, concentration, wear resistance and durability of the reinforce elements [1]. However, matrix wear resistance could be the key factor of detail working capacity in abrasive wear conditions.

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In these work is shown the hardness and wear resistance research results of the metal which is surfaced whit the use of flux coder wire systems Fe-C-Si-Mn-Cr-Ni-Mo-V and Fe-C-Si-Mn-Ni-Mo-W-V.

Flux cored wire manufacturing was conducted on laboratory machine. Diameter of powder wire is 5mm, wire shell is made from metal ribbon of St3 grade. As a filler were used corresponding powder materials: iron powder brand PJV 1 by GOST 9849-86, ferrosilicon powder brand FS 75 by GOST 1415-93, powder of high carbon ferrochrome brand FH900A by GOST 4757-91, powder of carbon ferromanganese FMn 78(A) by GOST 4755-91, nickel powder PNK-1L5 by GOST 9722-97, ferromolybdenum powder brand FM060 by GOST 4759-91, tungsten powder brand PVP-1 by

TI 48-19-71-78, ferrovanadium powder brand FV50U 0.6 by GOST 27130-94, cobalt powder brand PK-1U2 by GOST 9721-79. As a carbon-contained component was used carbon-fluorine contain material (CFCM) that was previously used in works [18-21] with the following chemical composition, wt.%: Al₂O₃ = 21-46.23; F = 18-27; Na₂O = 8-15; K₂O = 0.4-6; CaO = 0.7-2.3; Si₂O = 0.5-2.48; Fe₂O₃ = 2.1-3.27; C_{obsh} = 12.5-30.2; MnO = 0.07-0.9; MgO = 0.06-0.9; S = 0.09-0.19; P = 0.1-0.18.

Surfacing under the AN-26S flux was conducted in 6 layers on samples of the 09G2S grade steel with its 16mm thickness. Prosses was conducted with the use of automatic welding machine ASAW-1250 under following welding conditions: I_w =500 A; U_a = 30 V; V_w =9 meter per hour.

Hardness of the researched samples was measured with the use of hardness meter MET-DU. Hardness measurements were performed 5 times on the surface of each sample. In table 1 is shown average value of surfaced metal hardness measurements. Wear resistance tests were conducted no the laboratory machine 2070 SMT – 1. Wear tests were conducted as per flowchart rotating disk – sample. The disk has tungsten allow hard surface. Every test took 6 hours with rotation frequency 20 revolutions per minute. Before and after wear tests the samples were weighted to define the difference between initial and final weight, and the disk revolution amount of each test was noted. The wearout intensity was calculated in terms of weight reducing in one revolution of the disk.

Metallographic analysis was conducted on optical microscope OLYMPUS GX-51 in the light field in the limits of range $\times 100-1000$ magnification after etching samples by nital to determine the degree of influence changes in chemical composition on parameters of the microstructure. Studying of longitudinal deposited metal samples on nonmetallic inclusions existence was conducted in according with GOST 1778-70 with $\times 100$ magnification. Size of former austenite grain was determined by GOST 5639-56 with $\times 100$ magnification. Martensite needles size was determined by GOST 8233-56 with $\times 1000$ magnification.

Results and Discussion

Hardness, wear intensity tests results and chemical composition analysis of the samples is shown in table 1.

	Components weight content %							Sample	Sample wear	
Sample number	C	Si	Mn	Cr	Ni	Мо	V	W	hardness, HRC	intensity, grams per revolution * 10 ⁻⁴
1	0.23	0.12	0.85	1.45	0.53	0.51	0.68	0.08	25	1.65
2	0.21	0.23	0.89	1.45	0.54	0.55	0.54	0.03	21	1.15
3	0.17	0.18	0.85	1.40	0.52	0.54	0.63	0.05	21	1.11
4	0.17	0.28	0.91	1.32	0.45	0.46	0.59	0.06	21	1.12
5	0.15	0.20	0.79	0.08	0.56	0.25	0.51	3.38	17	1.15
6	0.14	0.17	0.75	0.07	0.5	0.13	0.47	2.57	16	4.08
7	0.14	0.26	0.78	0.09	0.55	0.68	0.56	2.88	16	1.70
8	0.12	0.21	0.71	0.07	0.52	0.5	0.44	2.43	15	1.79

Table 1 – Chemical composition, hardness, and wear intensity of the deposited metal.





Metallographic analysis of the samples which were surfaced by flux cored wire system Fe-C-Si-Mn-Cr-Ni-Mo-V shown, that when carbon contain is 0.17-0.23% and chromium contain is within the limits 1.30-1.50% (samples No1-4) it provides uniform structure with fine-needled martensite (rating No3) which is formed inside the borders of the former austenite grain, retained austenite, which is presented in small amounts in the form of separate islands, and thin layers of δ -ferrite, which is located on the borders of the former grain austenite (Fig. 1). Martensite needle size in the structure of the researched samples is in ranges 2-5 mcm (table 2). Size of former austenite grain conforms N_{26} .

Use of CFCM as a carbon contain component provided high metallurgical quality of the surfaced metal. Nonmetallic inclusions impurity of all researched samples is inconspicuous: low amount of tiny nonmetallic inclusions was established, particularly non-deformable silicates and oxide spots (table 2).

Sapmle number	The contamination inclusion	on of nonmetallic ns, rating	Size of	Size of martensite needles, mcm	
	Non-deformable silicates (fragile)	Oxide spots	rating		
1	1b, 2b, 3a	1a	6, 5	2-5	
2	1b, 2b, 3a	1a, 2a	6	2-4	
3	1b, 2b, 3a	1a	6	2-5	
4	1b, 2b, 3a	1a	6	2-4	
5	2b, 1b, 2a	1a	4, 5	-	
6	2b, 1b, 2a	1a	4, 5	-	
7	1b, 2b, 2a	1a	4	-	
8	2b, 3b	1a	4	-	

Table 2 – Nonmetallic inclusions and structure characteristics of researched samples.

It is established, that chromium contains in the deposited layer in 1.32-1.45% amount, bars from growing austenite grain during surfacing prosses and, consequently, promotes forming fine-needled martensite structure during metal cooling, that is confirmed by better rating of hardness and wear resistance in comparison with samples which are surfaced by the wire with higher tungsten contain (table 1).

Metallographic analysis of metal surfaced by flux cored wire system Fe-C-Si-Mn-Ni-Mo-W-V shown, that appending tungsten in amount 2.43-3.38% while reducing carbon and chromium contain down to 0.12-0.15% and 0.07-0.09%, consequently produce forming hypopearlitic structure in the deposited layer (Fig. 2).

Samples No4-8 has hypopearlitic structure with former austenite grain size No4, No5. What is more, there is big amount of retained austenite in the structure, that is located on boundaries of pearlite grain colonies. Also, is noticed presence of fine black inclusions in the boundaries of pearlite grain colonies, what is characteristically for tungsten carbides. Assigned structure changes determine reducing of deposited metal hardness and wear resistance (table 2).

With that said, established, that, despite tungsten carbides presence in hypopearlitic structure of the samples, which was surfaced by low-carbon flux cored wire system Fe-C-Si-Mn-Ni-Mo-W-V, more suitable and preferable for surfacing equipment details and mechanisms, that works in abrasive wear conditions, is flux cored wire system Fe-C-Si-Mn-Cr-Ni-Mo-V. Apparently, hypopearlitic matrix could not provide enough good counterstand against abrasive wear because of lower hardness, so formed tungsten carbides could not fully provide wear resistance, because they require more hard matrix for rigid adherence. Consequently, the conclusion is that hypopearlitic structure is not preferable to incorporate it with tungsten carbides to increase wear resistance.



a, b – sample №5; c, d – sample №6; e, f – sample №7; g, h – sample №8
Fig. 2 – Microstructure of the metal deposited by the flux cored wire system Fe-C-Si-Mn-Ni-Mo-W-V, (a, c, e, g × 100), (b, d, f, h × 500).

Conclusions

1. Established, that using lean alloyed flux cored wires of the systems Fe-C-Si-Mn-Cr-Ni-Mo-V and Fe-C-Si-Mn-Ni-Mo-W-V with the use as a carbon contain component CFCM provides forming deposited layers with low nonmetallic impurity level.

2. Using flux cored wire of the system Fe-C-Si-Mn-Cr-Ni-Mo-V for surfacing provides forming in the deposited layer uniform fine-needled martensite structure with thin layers of δ -ferrite and

former austenite, that supply enough hardness and wear resistance for miner equipment details exploitation.

3. Using flux cored wire of the system Fe-C-Si-Mn-Cr-Ni-Mo-V provides obtaining deposited layers with lower carbon and chromium contain, but higher tungsten contain, that leads forming not martensite, but hypopearlitic structure with tungsten carbides, which could not supply requiring hardness and wear resistance level.

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